# Closed-Form Design of Maxflat R-Regular IIR Mth-Band Filters

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#### 1 Introduction

Mth-band filters are an important class of digital filters and have found numerous applications in multirate signal processing systems, filter banks and wavelets [1]. This paper considers the design problem of maxflat R-regular IIR Mth-band filters, and gives the closed-form expression for its filter coefficients. The filter coefficients are directly derived by solving a linear system of Vandermonde equations, which are obtained from the regularity condition of the maxflat R-regular Mth-band filters via the blockwise waveform moments.

## 2 IIR Mth-Band Filters

Let  $h_n$   $(0 \le n < \infty)$  be an impulse response of IIR digital filter H(z). If H(z) is a *M*th-band filter, its impulse response is required to be exactly zero-crossing except for one point K, i.e.,

$$h_{K+mM} = \begin{cases} \frac{1}{M} & (m=0) \\ 0 & (m=\pm 1, \pm 2, \cdots) \end{cases},$$
(1)

where K and M are integers, and K corresponds to the desired group delay in the passband.

Mth-band filter is required to be lowpass, and the desired frequency response is given by

$$H_d(e^{j\omega}) = \begin{cases} e^{-jK\omega} & (\omega \in \text{passband}) \\ 0 & (\omega \in \text{stopband}) \end{cases}$$
(2)

Let a noncausal shifted version of H(z) be  $\hat{H}(z) = z^{K}H(z)$ , i.e.,  $\hat{h}_{n} = h_{n+K}$ . The desired frequency response of  $\hat{H}(z)$  becomes

$$\hat{H}_d(e^{j\omega}) = \begin{cases} 1 & (\omega \in \text{passband}) \\ 0 & (\omega \in \text{stopband}) \end{cases}$$
(3)

By using the polyphase representation, we have

$$H(z) = \sum_{i=0}^{M-1} z^{-i} H_i(z^M), \qquad (4)$$

where

$$H_i(z) = \sum_{n=0}^{N_1^i} a_n^i z^{-n} / \sum_{n=0}^{N_2^i} b_n^i z^{-n}, \qquad (5)$$

where  $N_1^i, N_2^i$  are the degree of the numerator and denominator, respectively,  $a_n^i, b_n^i$  are real filter coefficients, and  $b_0^i = 1$ . Assume that  $K = L_1M + L_2$ , where  $L_1, L_2$  are integers, and  $0 \le L_2 \le M - 1$ , it can be seen from the timedomain condition in (1) that  $H_{L_2}(z) = z^{-L_1}/M$ . Therefore, we have

$$\hat{H}(z) = z^{K} H(z) = \frac{1}{M} + \sum_{\substack{i=0\\ \neq L_{2}}}^{M-1} z^{K-i} H_{i}(z^{M}).$$
(6)

It can be seen from (6) that the frequency response of  $\hat{H}(z)$  always satisfies

$$\sum_{k=0}^{M-1} \hat{H}(e^{j(\omega + \frac{2k\pi}{M})}) \equiv 1,$$
(7)

which means that the sum of the responses at the frequency points  $\omega_k = \omega + 2k\pi/M$  for  $k = 0, 1, \dots, M-1$  keep constant, regardless of what the filter coefficients are. From (7), we get

$$\hat{H}(e^{j\omega_0}) = 1 - \sum_{k=1}^{M-1} \hat{H}(e^{j\omega_k}).$$
(8)

It is clear that the frequency response at  $\omega_0$  is dependent on the frequency responses at  $\omega_k$   $(k = 1, 2, \dots, M - 1)$ . If its stopband response is 0, then the frequency response of  $\hat{H}(z)$  will become 1 in the passband, i.e., the magnitude response of H(z) is 1, and the group delay is K in the passband. Therefore, the design problem of IIR Mth-band filters with an arbitrarily specified K can be reduced to the minimization of the stopband error of  $\hat{H}(z)$ .

#### 3 Maxflat *R*-regular IIR *M*th-band Filters

In [5], the blockwise waveform moment around K for  $h_n$  is defined by

$$m_r(i) = \sum_{m=0}^{\infty} (mM + i - K)^r h_{mM+i},$$
 (9)

where  $0 \leq i \leq M-1$ . It follows from the definition of  $m_r(i)$  that

$$\left. \frac{\partial^r \hat{H}(e^{j\omega})}{\partial \omega^r} \right|_{\omega = \frac{2k\pi}{M}} = (-j)^r \sum_{i=0}^{M-1} m_r(i) e^{-j\frac{2(i-K)k\pi}{M}}, \quad (10)$$

i.e., the blockwise waveform moments describe the derivative behaviors of the frequency response  $\hat{H}(e^{j\omega})$  at the frequency points  $\omega_k = 2k\pi/M$  ( $0 \le k \le M - 1$ ). It is seen in (10) that the *r*th derivatives of the frequency response  $\hat{H}(e^{j\omega})$  at  $\omega_k = 2k\pi/M$  are the *M*-point DFT (Discrete Fourier Transform) of the blockwise waveform moments  $m_r(i)$ . Thus, by the inverse transform, we have

$$m_r(i) = \frac{j^r}{M} \sum_{k=0}^{M-1} \left. \frac{\partial^r \hat{H}(e^{j\omega})}{\partial \omega^r} \right|_{\omega = \frac{2k\pi}{M}} e^{j\frac{2(i-K)k\pi}{M}}.$$
 (11)

It is clear that the blockwise waveform moments  $m_r(i)$  bridge between the time and frequency domains by (9) and (11). Given the *r*th derivatives of the frequency response  $\hat{H}(e^{j\omega})$  at the frequency points  $\omega_k = 2k\pi/M$ , the *r*th blockwise waveform moments  $m_r(i)$  can be calculated via the IDFT in (11).

It is known in [1] that an Mth-band filter is said to be R-regular if it has

$$H(z) = (1 + z^{-1} + \dots + z^{-(M-1)})^R Q(z), \qquad (12)$$

where Q(z) is an IIR filter. It is equivalent to

$$\frac{\partial^r H(e^{j\omega})}{\partial \omega^r} \bigg|_{\omega = \frac{2k\pi}{M}} = \frac{\partial^r \dot{H}(e^{j\omega})}{\partial \omega^r} \bigg|_{\omega = \frac{2k\pi}{M}} = 0, \quad (13)$$

for  $k = 1, 2, \dots, M-1$  and  $r = 0, 1, \dots, R-1$ . It is obtained from (8) and (13) that

$$\begin{cases} \hat{H}(e^{j\omega})\big|_{\omega=0} &= 1 \quad (r=0) \\ \frac{\partial^r \hat{H}(e^{j\omega})}{\partial \omega^r}\Big|_{\omega=0} &= 0 \quad (r=1,2,\cdots,R-1) \end{cases}, (14)$$

which means that the magnitude response  $|\hat{H}(e^{j\omega})|$  and group delay  $\hat{\tau}(\omega)$  satisfy at  $\omega = 0$ 

$$\begin{cases} \left| \hat{H}(e^{j\omega}) \right| \Big|_{\omega=0} &= 1 \quad (r=0) \\ \left. \frac{\partial^r \left| \hat{H}(e^{j\omega}) \right|}{\partial \omega^r} \right|_{\omega=0} &= 0 \quad (r=1,2,\cdots,R-1) \end{cases},$$
(15)

and

$$\frac{\partial^r \hat{\tau}(\omega)}{\partial \omega^r} \Big|_{\omega=0} = 0 \qquad (r=0,1,\cdots,R-2).$$
(16)

From the relationship between H(z) and  $\hat{H}(z)$  in (6), it is clear that H(z) has flat magnitude and group delay responses at  $\omega = 0$  simultaneously.

By using (11), the blockwise waveform moments are obtained from the regularity condition in (13) and (14) as

$$m_r(i) = \begin{cases} \frac{1}{M} & (r=0) \\ 0 & (r=1,2,\cdots,R-1) \end{cases}$$
(17)

It can be obtained from (5) that

$$z^{K-i}H_i(z^M) = \frac{\sum_{n=0}^{N_1^i} a_n^i z^{K-nM-i}}{\sum_{n=0}^{N_2^i} b_n^i z^{-nM}} = \sum_{m=0}^{\infty} h_{mM+i} z^{K-mM-i}.$$
(18)

Next, we define the waveform moments for the numerator and denominator in (18) by

$$\begin{cases} m_r^N(i) = \sum_{n=0}^{N_1^i} (nM + i - K)^r a_n^i \\ m_r^D(i) = \sum_{n=0}^{N_2^i} (nM)^r b_n^i \end{cases}$$
(19)

Therefore, it can be seen by taking rth derivatives of (18) and substituting z = 1 that the condition in (17) becomes

$$Mm_r^N(i) = m_r^D(i)$$
  $(r = 0, 1, \cdots, R-1).$  (20)

From the definition of  $m_r^N(i), m_r^D(i)$  in (19) and  $b_0^i = 1$ , we obtain

$$M\sum_{n=0}^{N_1^i} (nM+i-K)^r a_n^i - \sum_{n=1}^{N_2^i} (nM)^r b_n^i = \delta(r), \qquad (21)$$

where  $r = 0, 1, \cdots, R - 1$ , and

$$\delta(r) = \begin{cases} 1 & (r=0) \\ 0 & (r\neq 0) \end{cases} .$$
 (22)

It should be noted that the coefficient matrix in (21) is the Vandermonde matrix with distinct elements. There is always a unique solution if  $R = N_1^i + N_2^i + 1$ . By using the Cramer's rule, we can obtain the presentation of the filter coefficient as a quotient of two Vandermonde's determinants. Therefore, a closed-form solution is obtained as

$$\begin{cases} a_n^i = \frac{(-1)^{n+1}}{M} \frac{N_2^i!}{n!(N_1^i - n)!} \frac{\prod_{m=0}^{N_1^i} (m + \frac{i - K}{M})}{\prod_{m=0}^{N_2^i} (m - n + \frac{K - i}{M})} \\ b_n^i = (-1)^n \frac{N_2^i!}{n!(N_2^i - n)!} \prod_{m=0}^{N_1^i} \frac{m + \frac{i - K}{M}}{m - n + \frac{i - K}{M}} \end{cases}$$

$$(23)$$

Once M, K,  $N_1^i$  and  $N_2^i$  are given, a set of filter coefficients  $a_n^i$  and  $b_n^i$  can be easily calculated by using (23). It is seen that besides  $N_1^i + N_2^i = R - 1$  must be satisfied, it is possible for  $H_i(z)$  to have different  $N_1^i$  and  $N_2^i$  for  $0 \le i \le M - 1$ .

### 4 Conclusion

In this paper, we have proposed a new closed-form solution for the maxflat R-regular IIR Mth-band filters. The filter coefficients have been directly derived by solving a linear system of Vandermonde equations, which are obtained from the regularity condition via the blockwise waveform moments.

#### References

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